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Research Article

Optimal Management of a Double-Fed Induction Generator Using Feedback Linearization: Suggestions and Prospects

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Abstract

Recommendations for feedback linearization in DFIG control include incorporating cutting-edge methods like soft computing, increasing performance for ancillary services and maximum power point tracking (MPPT), and enhancing control performance under fluctuating wind and grid disturbances. Future directions call for creating more resilient and flexible nonlinear controllers to manage intricate MIMO systems, integrating feedback linearization with other control techniques like intelligent control algorithms and fractional order controllers, and making it possible to control DFIGs in hybrid energy systems to better manage multiple energy sources. Nevertheless, there are disadvantages as well, like heightened computational complexity and possible susceptibility to model errors.

Keywords: *Recommendations, Impacts, DFIG-WT, Maximum Power Point Tracking, Feedback linearization, Future Directions.*

I. Introduction

Power generation from renewable energy is ever growing due to global warming disquiets, hikes in oil prices, and government policies towards clean energy [1-3]. The fastest-growing source of renewable energy is wind power. The power is generated when the wind speed is enough to rotate the blades of the turbine. The mechanical energy of the rotating blades is converted to electricity by a generator. The preferred location of wind farms is offshore sites where the wind is stronger. Offshore wind farms generate sustainable energy in large quantities, contrary to land wind farms [4]. At the moment, the doubly-fed induction generator (DFIG) is predominantly used for offshore applications. The main advantages of DFIG for this application are generating power at low wind speed, generating power at constant frequency and voltage even though the rotor speed is varying, maintaining unity power factor, revamped efficiency, and cost-effectiveness [5-7]. DFIG has both rotor and stator windings. The rotor windings are connected to the grid via back-to-back converters. The back-to-back converters are responsible for regulating both the grid and the rotor currents. Rotor current regulation makes it possible to regulate the active and reactive powers fed to the load from the stators, and this is independent of the rotor speed [8, 9]. The stator windings are directly connected to the grid by means of the tertiary winding of the transformers. The control of DFIG is more complex than that of a traditional induction generator. The operation of DFIG can be drastically affected by the capricious wind speed if there were no control system incorporated into it. Similarly, incessant connection of loads to the electrical system by the consumers of electricity can severely affect the DFIG system without any control [11]. Over the years, many researchers have come up with numerous control techniques to make the DFIG system robust, such as well as be able to handle any undesired disturbance it may encounter. The most common of such techniques is conventional vector control. It allows separate control of active and reactive power based on the assumptions that the stator flux is constant and the stator resistance is negligible [12, 13]. This method suffers a huge setback under grid fault or when the wind speed is varying. As a result, the stator flux is no longer constant. Furthermore, the dynamics of vector control solely depend on the fine-tuned gains of the proportional-integral (PI) controller. However, selecting such gains to ensure stability under varying load is arduous [14]. Moreover, a PI controller is applied in [15] to control the grid-side converter of DFIG. Further improvement upon this, a fuzzy logic-based controller has been designed in [16] to smoothen the output power oscillation from the grid-side converter. Model Predictive Controller (MPC) can conquer the aforementioned limitation of the PI controller and offer an excellent solution for current, flux, power, and torque control [17]. MPC is easier to design, cost-effective, and has a faster response than a PI controller. Nevertheless, coordinate MPC controllers for rotor-side converters (RSCs) and stator-side converters (SSCs) hardly have any significant improvement on the performance of DFIG [14]. Linear Quadratic Regulator (LQR) based on optimal control has been implemented in [18] for pitch control of DFIG wind turbines. The performance of the LQR pitch control is more effective in comparison to PI pitch control. [19] employed Genetic Algorithm (GA) to obtain optimal matrices. The overall performance of this controller is superior to that in [18]. The aforementioned control techniques are based on the approximated linear model of DFIG near a particular operating point. The controllers give satisfactory performances only near this point. As a result, these controllers are not suitable for DFIG in Wind Energy Conversion Systems (WECS). This is because DFIG is required to operate under variable speed and a wide range of operating points due to capricious wind speed. Therefore, nonlinear control techniques must be employed to cope with the nonlinearities in the system and achieve acceptable wind energy conversion. Nonlinear robust sliding mode control has been successfully applied in [20] to control the grid voltage. However, the chartering effect augments the mechanical wear. The chattering effect can be attenuated by using higher-order sliding mode [21]. Second-order sliding mode, also known as the super-twisting algorithm, has been applied in [22] to attain maximum power point tracking (MPPT). Furthermore, adaptive backstepping control capable of eliminating uncertainties in the system has been described in [23]. Backstepping approach for achieving

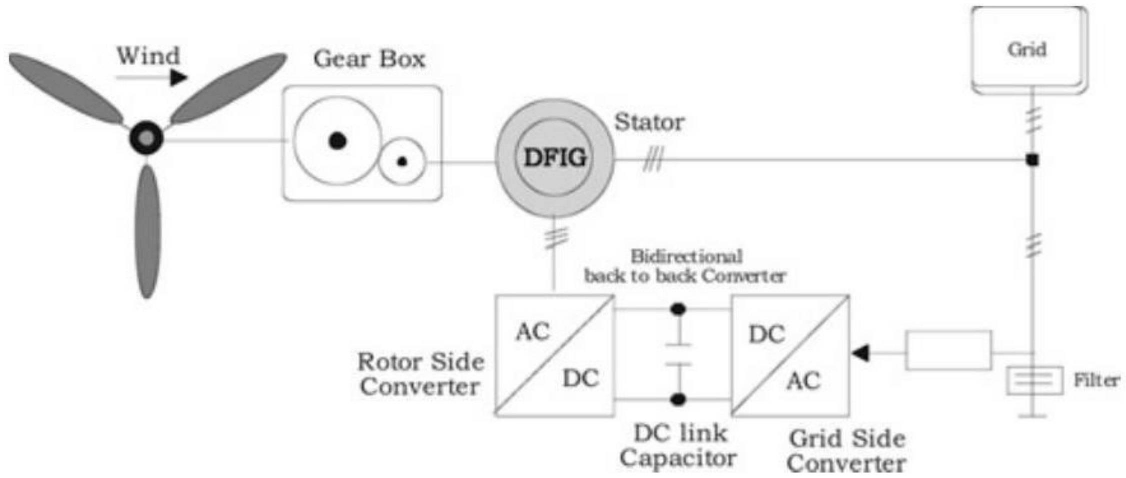

Fig. 1. Wind energy conversion system DFIG [10]
reference tracking has been implemented in [23] to control the rotor side converter.

Adaptive feedback linearization together with an observer for estimating model uncertainties was employed to improve the performance of wind turbine DFIG [24]. A decentralized feedback linearization controller has been proposed for wind turbine DFIG using differential geometry to improve the transient stability of the power system [25]. Feedback linearization control for the current loop was used to attain maximum power point tracking in [26]. The aforementioned nonlinear controllers were based on a reduced-order model of DFIG. The stator dynamics were ignored to reduce the order of the model. This greatly reduced the computational complexity and simplified control design at the expense of accuracy.In this paper, the full-order nonlinear model of DFIG together with the stator dynamics has been put into consideration to overcome the limitation of the aforementioned models. Furthermore, four inputs and four outputs of the DFIG are considered for control design, unlike the aforesaid. A feedback linearization controller has been proposed for input-output decoupling of the system to allow coordinated control of the rotor current and stator flux. This allows the speed to be regulated in such a way as to achieve maximum power point tracking. Model Predictive Controller (MPC) with output constraints has been designed for the rotor side to ensure that the rotor retains optimal speed for all operating points. It also improves the transient state of the rotor speed. The paper is organized as follows: In section I, the mathematical model of DFIG-WT has been derived. In section II, the proposed control schemes have been implemented in section III. The simulation results and the effectiveness of the proposed control schemes have been shown in section IV. The conclusion of the work has been carried out in section V. Also, the impacts and challenges of the feedback linearization-based model Predictive control of rotor speed of DFIG-WT is discussed in this research.

II. Recommendations for Current DFIG Control

1. Improve Performance Under Grid Disturbances:
   Utilize feedback linearization to design controllers that can accurately manage the DFIG system's performance, especially under unbalanced voltage conditions, as shown in a study by IEEE Xplore.
2. Enhance Ancillary Services and Profitability:
   Develop feedback linearization-based schemes that can simultaneously provide both power regulation (active and reactive) for grid operators and optimize profit for wind park operators by maximizing power output, as outlined by ResearchGate.
3. Optimize Power Tracking:
   Integrate feedback linearization with advanced techniques like enhanced Maximum Power Point Tracking (MPPT) and Lyapunov functions to achieve better power output from the DFIG system, particularly under varying wind speeds, according to a publication by MDPI [36].

III. Future Directions for Feedback Linearization

1. Adaptive and Robust Control:
   Explore more adaptive and robust nonlinear control schemes that can handle the inherent nonlinearities and uncertainties in DFIG systems, especially in the presence of significant wind gusts and other environmental factors.
2. Integration with Soft Computing:
   Combine feedback linearization with intelligent control methods, such as soft-computing-assisted fractional-order controllers, to improve control accuracy, response time, and overall system stability.
3. Hybrid Energy System Management:
   Extend feedback linearization to manage hybrid energy conversion systems, which may include wind, solar (PV), and other sources, for more comprehensive and efficient energy management.
4. MIMO Control Strategies:
   Focus on designing more sophisticated multi-input multi-output (MIMO) feedback linearization controllers to manage the coupled dynamics of DFIGs more effectively, leading to superior performance in complex wind turbine systems [36].

IV. Advantages of the Feedback Linearization Based Model Predictive Control of Rotor Speed of DFIG-WT

i. Handles Nonlinearities:
   FBL transforms the nonlinear DFIG model into a linear one, making it easier to apply MPC, which is typically designed for linear systems. This allows for better control performance in the presence of wind speed variations and other nonlinearities inherent in wind turbines.

ii. Constraint Handling:
   MPC, with or without FBL, can explicitly handle constraints on rotor speed, currents, and other system variables, leading to more robust and safer operation.

iii. Performance Improvement:
   Compared to traditional controllers like PI regulators, FBL-based MPC can achieve better performance in terms of tracking speed, stability, and power quality.

iv. Flexibility:
   FBL-based MPC can be adapted to various wind turbine configurations and operating conditions by adjusting the model and constraints within the MPC framework.

v. Reduced Computational Complexity (compared to pure nonlinear MPC):
   FBL simplifies the online solution of the complex optimization problem in nonlinear MPC, making it more feasible for real-time implementation [36].

V. Disadvantages of the Feedback Linearization Based Model Predictive Control of Rotor Speed of DFIG-WT

i. Model Dependence:
   FBL relies on an accurate mathematical model of the DFIG. Inaccuracies in the model can lead to performance degradation or even instability.

ii. Increased Computational Burden:
   While FBL reduces the computational burden of nonlinear MPC, it still involves more complex calculations than linear MPC or traditional controllers, potentially requiring more powerful processing units.

iii. Sensitivity to Parameters:
   The effectiveness of FBL-based MPC can be sensitive to uncertainties in system parameters, requiring careful parameter tuning or robust control design.

iv. Complexity of Implementation:

Implementing FBL-based MPC can be more challenging than simpler control strategies due to the need for understanding and implementing the feedback linearization technique and the MPC algorithm.

v. Potential for Oscillations:
If not properly tuned, the control loop can exhibit oscillations, especially during transient conditions or when dealing with uncertainties.

vi. Additional Hardware:
In some cases, additional hardware like static synchronous compensators (STATCOMs) or dynamic voltage restorers (DVRs) might be needed to improve grid support during faults, adding to the system's complexity and cost [35].

VI. Mathematical Modelling of DFIG

The schematic diagram of the DFIG is depicted in Fig. 1. The full order mathematical model of DFIG-WT in direct and quadrature dq- synchronization frame can be derived as [27, 28]. Application of Kirchhoff's voltage and current laws at all the loops and the nodes of the dq-equivalent circuit diagram [27], the following equations are derived.

$$\frac{d\Psi_{sd}}{dt} = \omega_1 \Psi_{sq} - R_s i_{sd} + u_{sd} \tag{1}$$

$$\frac{d\Psi_{sq}}{dt} = \omega_1 \Psi_{sd} - R_s i_{sq} + u_{sq} \tag{2}$$

$$\frac{d\Psi_{rd}}{dt} = \omega_s \Psi_{rq} - R_r i_{rd} + u_{rd} \tag{3}$$

$$\frac{d\Psi_{rq}}{dt} = \omega_s \Psi_{sd} - R_r i_{rq} + u_{rq} \tag{4}$$

$$\frac{d\omega_r}{dt} = \frac{n_p}{J}(T_e - T_m) \tag{5}$$

(6)

$$\Psi_{sd} = L_m i_{rd} + L_s i_{sd} \tag{7}$$

$$\Psi_{sq} = L_m i_{rq} + L_s i_{sq} \tag{8}$$

$$\Psi_{rd} = L_m i_{sd} + L_r i_{rd} \tag{9}$$

$$\Psi_{rq} = L_m i_{sq} + L_r i_{rq} \tag{9}$$

$$T_e = \frac{3L_m n_p}{2L_s}\left(\Psi_{sd} i_{rq} - \Psi_{sq} i_{rd}\right) \tag{9}$$

Where:

u_{sd}, u_{sq}	d-q components of stator voltage
i_{sd}, i_{sq}	d-q components of stator current
Ψ_{sd}, Ψ_{sq}	d-q components of stator flux
$u_{rd},\ u_{rq}$	d-q components of rotor voltage
$i_{rd},\ i_{rq}$	d-q components of rotor current
$\Psi_{rd},\ \Psi_{rq}$	d-q components of rotor flux
R_s, R_r	Rotor and stator resistances respectively
L_m, L_r and L_s	Mutual, rotor and stator inductances respectively
J	Generator rotational inertia
T_e	Electromagnetic torque
n_p	Number of pairs of poles

Further evaluations and transforming the state variables, the dynamic equations can be written in the form

$$\dot{x}_1 = -a_1x_1 + a_2x_2 + a_3x_3 + u_1 \quad (10)$$
$$\dot{x}_2 = -a_2x_1 - a_1x_2 + a_3x_4 + u_2 \quad (11)$$
$$\dot{x}_3 = a_4x_1 - a_5x_2x_5 - a_6x_3 + a_7x_4 - a_5u_1 + a_{10}u_3 \quad (12)$$
$$\dot{x}_4 = a_5x_1x_5 + a_4x_2 - a_7x_3 - a_6x_4 - a_5u_2 + a_{10}u_4 \quad (13)$$
$$\dot{x}_5 = a_8(x_1x_4 - x_2x_3) - a_9 \quad (14)$$
$$y_1 = x_1 \quad (14)$$
$$y_2 = x_2 \quad (14)$$
$$y_3 = x_4 \quad (14)$$
$$y_4 = x_5 \quad (14)$$

The nonlinear differential equations can be written in normal form:

$$\begin{cases} \dot{x} = f(x) + g(x)u \\ y = h(x) \end{cases} \quad (15)$$

Where:

$$x = [x_1 \quad x_2 \quad x_3 \quad x_4 \quad x_5]^{\top} = [\Psi_{sd} \quad \Psi_{sq} \quad i_{rd} \quad i_{rq} \quad \omega_r]^{\top}$$
$$u = [u_1 \quad u_2 \quad u_3 \quad u_4]^{\top} = [u_{sd} \quad u_{sq} \quad u_{rd} \quad u_{rq}]^{\top}$$
$$y = [h_1(x) \quad h_2(x) \quad h_3(x) \quad h_4(x)]^{\top} = [x_1 \quad x_2 \quad x_4 \quad x_5]^{\top}$$

$$f(x) = \begin{bmatrix} -a_1x_1 + a_2x_2 + a_3x_3 \\ -a_2x_1 - a_1x_2 + a_3x_4 \\ a_4x_1 - a_5x_2x_5 - a_6x_3 + a_7x_4 \\ a_5x_1x_5 + a_4x_2 - a_7x_3 - a_6x_4 \\ a_8(x_1x_4 - x_2x_3) - a_9 \end{bmatrix}$$

$$g(x) = \begin{bmatrix} 1 & 0 & 0 & 0 \\ 0 & 1 & 0 & 0 \\ -a_5 & 0 & a_{10} & 0 \\ 0 & -a_5 & 0 & a_{10} \\ 0 & 0 & 0 & 0 \end{bmatrix}$$

$a_1 = \frac{R_s}{L_s}$, $a_2 = \omega_1$, $a_3 = \beta R_s$, $a_4 = \frac{\beta R_s}{\alpha L_s}$, $a_5 = \frac{\beta}{\alpha}$, $a_6 = \frac{R_r + \beta^2 R_s}{\alpha}$, $a_7 = \omega_s$, $a_8 = \frac{3L_m n_p^2}{2JL_s}$, $a_9 = \frac{n_p}{J}T_m$, $a_{10} = \frac{1}{\alpha}$, $\alpha = \frac{(L_rL_s - L_m^2)}{L_s}$, $\beta = \frac{L_m}{L_s}$

VII. Control Design

In this section, the proposed controller scheme is presented. The objective is to regulate the speed to an optimal value by coordinated control of rotor current and stator flux.

A. Maximum power point tracking

The amount of power a wind turbine can capture from the wind is given by [26]:

$$p = \frac{1}{2}\rho\pi R_{wt}^2 C_p(\lambda, \theta) V_{wind}^3 \quad (16)$$

$$\lambda = \frac{\omega_r R_{wt}}{K_1 V_{wind}} \quad (17)$$

The power coefficient is a function of both pitch angle θ and tip speed ratio λ defined by [27]:

$$C_p(\lambda,\theta) = 0.5176\left(\frac{116}{\lambda_j} - 0.4\theta - 5\right)e^{\frac{-21}{\lambda_j}} + 0.0068\lambda \tag{18}$$

$$\frac{1}{\lambda_j} = \frac{1}{\lambda_j + 0.08\theta} - \frac{0.035}{\beta^3 + 1} \tag{19}$$

Where ρ is air density, R_{wt} is radius of wind turbine, V_{wind} is wind speed, $C_p(\lambda,\theta)$ is power coefficient, θ is pitch angle and λ is tip speed ratio.

Wind turbine can generate maximum power provided that the power coefficient $C_p(\lambda,\theta)$ is maximum for any wind speed within the wide operation region of the turbine. The power coefficient $C_p(\lambda,\theta)$ can be maximized by maintaining optimal value of the tip speed ratio λ_{opt} and fixed pitch angle θ.

$$C_{p\max} = C_p(\lambda_{opt},\theta) \tag{20}$$

Therefore, the desired optimal speed is given by:

$$\omega_{rd} = \frac{K_1\lambda_{opt}}{R_{wt}}V_{wind} \tag{21}$$

B. Feedback linearization

the nonlinear MIMO system is decoupled and linearized based on input-output feedback linearization technique. The output of the system, y_k, is differentiated until the input, u_k, ($k = 1,2,3,4$) appears [26].

$$y_k^{r_k} = L_f^{r_k}h_k + \sum_{k=1}^{n} L_{g_k}L_f^{r_k-1}h_k u_k;\ k = 1,2,3,4 \tag{22}$$

where $y_k^{r_k}$ denotes the $r_k th$-order derivative of y_k. Each y_k has a r_k. The relative degree of the system is the same as the number of states, $(r = 1+1+1+2 = 5 = n)$. The third state is an internal state whose stability is proved in the subsequent section. Evaluating the Lie derivatives in (22) leads to the system of equations expressed in the matrices below.

$$\begin{bmatrix}\dot{y}_1\\ \dot{y}_2\\ \dot{y}_3\\ \ddot{y}_4\end{bmatrix} = \begin{bmatrix}L_f h_1(x)\\ L_f h_2(x)\\ L_f h_3(x)\\ L_f^2 h_4(x)\end{bmatrix} + \begin{bmatrix}L_{g1}L_f^0 h_1(x) & L_{g2}L_f^0 h_1(x) & L_{g3}L_f^0 h_1(x) & L_{g4}L_f^0 h_1(x)\\ L_{g1}L_f^0 h_2(x) & L_{g2}L_f^0 h_2(x) & L_{g3}L_f^0 h_2(x) & L_{g4}L_f^0 h_2(x)\\ L_{g1}L_f^0 h_3(x) & L_{g2}L_f^0 h_3(x) & L_{g3}L_f^0 h_3(x) & L_{g4}L_f^0 h_3(x)\\ L_{g1}L_f^1 h_4(x) & L_{g2}L_f^1 h_4(x) & L_{g3}L_f ?^1\, h_4(x) & L_{g4}L_f^1 h_4(x)\end{bmatrix}\begin{bmatrix}u_1\\ u_2\\ u_3\\ u_4\end{bmatrix}$$

$$[\dot{y}_1 \quad \dot{y}_2 \quad \dot{y}_3 \quad \ddot{y}_4]^{\mathsf{T}} = A(x) + E(x)u$$

$$A(x) = \begin{bmatrix} -a_1x_1 + a_2x_2 + a_3x_3 \\ -a_2x_1 - a_1x_2 + a_3x_4 \\ a_5x_1x_5 + a_4x_2 - a_7x_3 - a_6x_4 \\ a_8[(-a_1 - a_6)x_1x_4 + (a_2 - a_7)(x_2x_4 + x_1x_3) \\ +(a_1 + a_6)x_2x_3 + a_4x_5(x_1^2 + x_2^2)] \end{bmatrix}$$

$$E(x) = \begin{bmatrix} 1 & 0 & 0 & 0\\ 0 & 1 & 0 & 0\\ 0 & -a_5 & 0 & a_{10}\\ q_1 & q_2 & q_3 & q_4 \end{bmatrix}$$

where $q_1 = 2a_8(x_4 + a_5x_2), q_2 = -2a_8(x_3 + a_5x_1)$, $q_3 = -2a_8a_{10}x_2$, and $q_4 = 2a_8a_{10}x_1$, and $\text{Det}(E(x)) = 2a_8x_2a_{10}^2 \neq 0$. Therefore, $E^{-1}(x)$ exists.

The stabilizing inputs for the input-output feedback linearization are defined by; $v = [v_1 \quad v_2 \quad v_3 \quad v_4]$. The linear decoupling between the input and output variables of the system is realized by the control input given below.

$$u = E^{-1}(x)(-A(x) + v) \tag{23}$$

Where:

$$[\dot{y}_1 \quad \dot{y}_2 \quad \dot{y}_3 \quad \ddot{y}_4]^\top = [v_1 \quad v_2 \quad v_3 \quad v_4]^\top$$

The control objective is to drive the system to point of maximum power required that the defined in the vector, $\eta^d = [\Psi_{sd}^d \quad \Psi_{sq}^d \quad i_{rq}^d \quad w_r^d] = [y_{1d} \quad y_{2d} \quad y_{3d} \quad y_{4d}]$, so that the equilibrium points are shifted to the origin. The error signals are defined as:

$$e = \eta^d - y$$

$$\begin{bmatrix} v_1 \\ v_2 \\ v_3 \\ v_4 \end{bmatrix} = \begin{bmatrix} \dot{y}_{1d} + K_{p1}e_1 + K_{i1}\int e_1 dt \\ \dot{y}_{2d} + K_{p2}e_2 + K_{i2}\int e_2 dt \\ \dot{y}_{3d} + K_{p3}e_3 + K_{i3}\int e_3 dt \\ \ddot{y}_{4d} + K_{p4}e_4 + K_{i4}\int e_4 dt \end{bmatrix}$$

$$\begin{cases} \ddot{e}_1 + K_{p1}\dot{e}_1 + K_{i1}e_1 = 0 \\ \ddot{e}_2 + K_{p2}\dot{e}_2 + K_{i2}e_2 = 0 \\ \ddot{e}_3 + K_{p3}\dot{e}_3 + K_{i3}e_3 = 0 \\ \dddot{e}_4 + K_{p4}\dot{e}_4 + K_{i4}e_4 = 0 \end{cases}$$

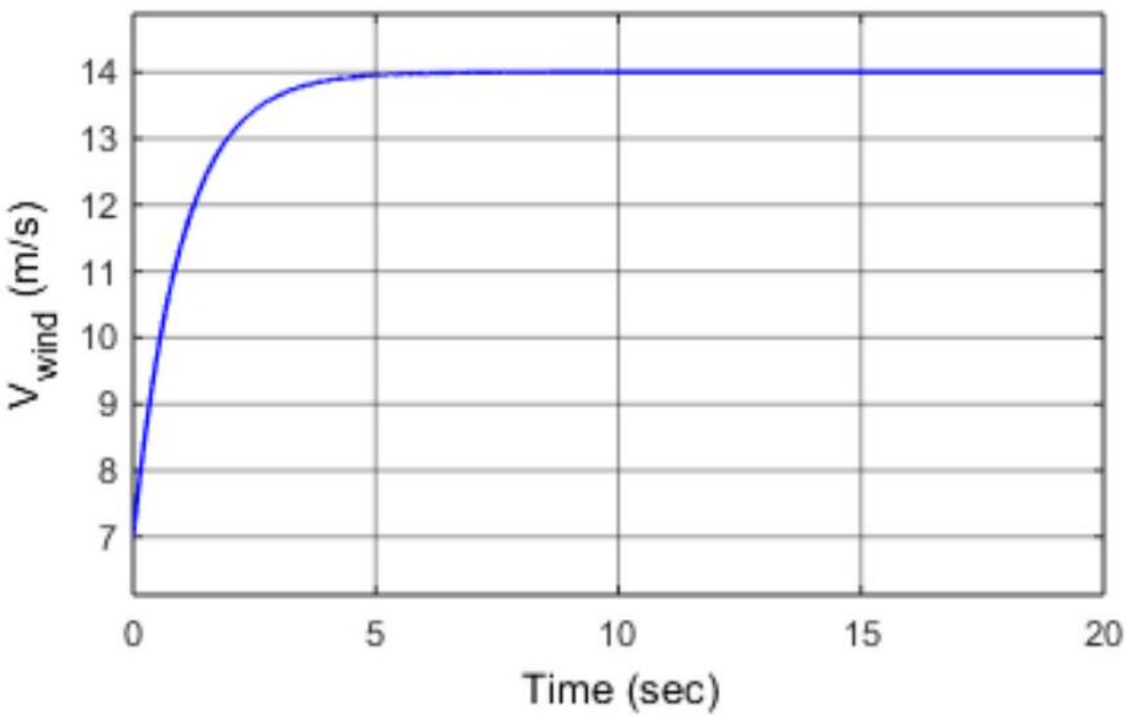

Fig. 2. Wind speed

C. Desired states of the controller

The control targets are the rotor current Ψ and stator flux. The stator oriented-flux frame is aligned with the q-axis. The reference values of the stator flux and its $d-q$ components are given by:

$$\Psi_{sd}^{d} = 0$$

$$\Psi_{sq}^{d} = \Psi^{d} = -\frac{V_s}{\omega_1} = -1$$

$$i_{rq}^{d} = -\frac{\Psi_s^d}{L_m} = -0.34$$

Where $\omega_1 = 1.0$pu is synchronous speed, $V_s = 1.0$pu is generator rated voltage,

The stabilizing inputs are selected in such a way that the errors converge to zero and the states x_1, x_2, x_4 and x_5 track the reference values $\Psi_{sd}^d, \Psi_{sq}^d, i_{rq}^d$ and w_r^d respectively.

VIII. Simulation Result

The performance of the proposed control schemes is evaluated in this section. The parameters of the DFIG-WT are obtained from [32].

The wind speed varies from 7 m/s to 14 m/s and then settles at 14 m/s as shown in Fig. 2. The control objective is to capture maximum power from this wind speed by maximizing the power coefficient and keeping the pitch angle fixed. The maximum power coefficient $\left(C_{pmax} = 9.0pu\right)$ is shown in Fig. 3 with the corresponding optimal tip-speed ratio $\left(\lambda_{\text{opt}} = 0.4569pu\right)$ at fixed pitch angle $\theta = 1.0$. The turbine will maintain optimal speed and subsequently maximum power as long as the power coefficient remains maximum.

The feedback linearization controller successfully decoupled the rotor and stator dynamics for proper coordinated control. The tuning parameters of the controller are $K_{p1} = 10, K_{i1} = 21, K_{p2} = 4, K_{i2} = 3.5, K_{p3} = 8, K_{i3} = 15, K_{p4} = 22, K_{i4} = 97$.

The d-component and the q-component of the stator flux are shown in Fig. 4 and Fig. 5, respectively. It can be seen that the components of the stator flux have tracked their respective desired values.

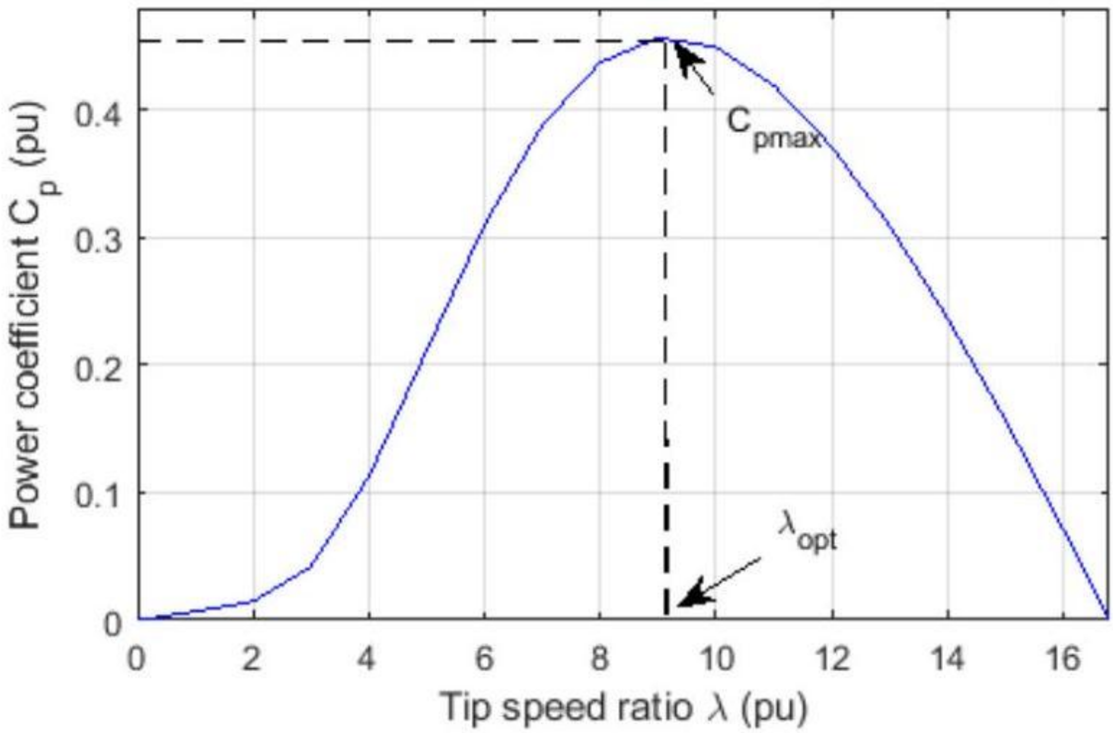

Fig. 3. Power coefficient vs tip-speed ratio

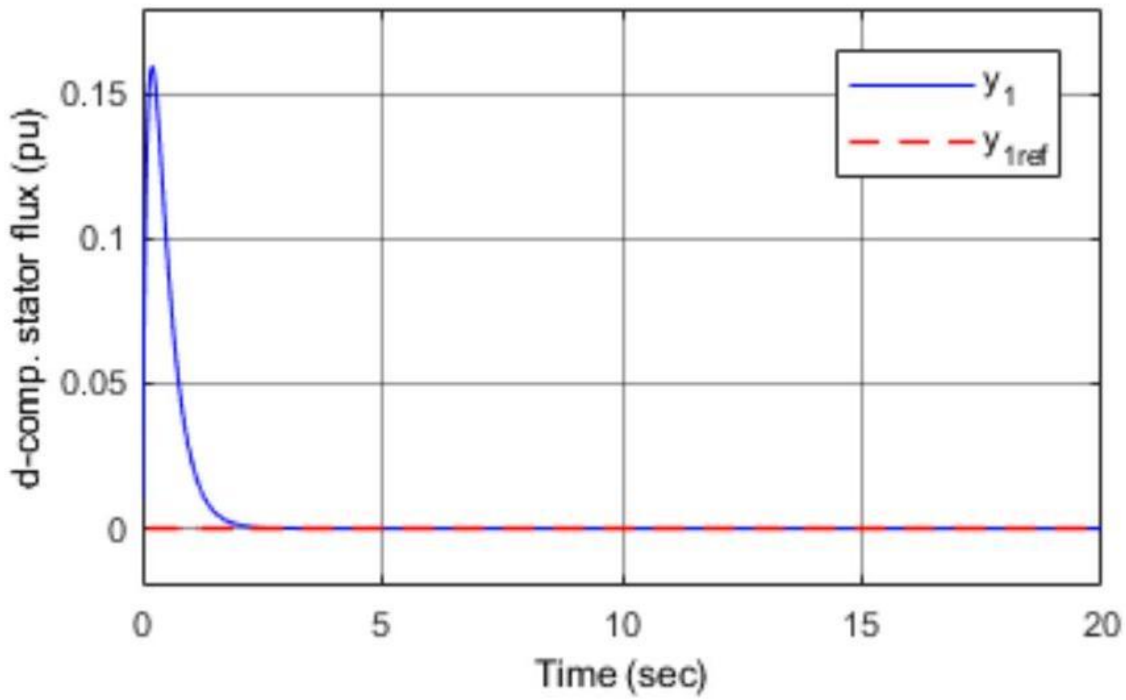

Fig. 4. d-component of stator flux

The q-component of rotor current (y_3) shown in Fig. 6. The speed can be regulated to the optimal speed for the maximum active power generation as shown in Fig. 7.

The tracking errors of the maximum power points converge to zero as shown in Fig. 8.

The control inputs to the DFIG-WT that decouple and ensure the maximum power generation are shown in Fig. 9.

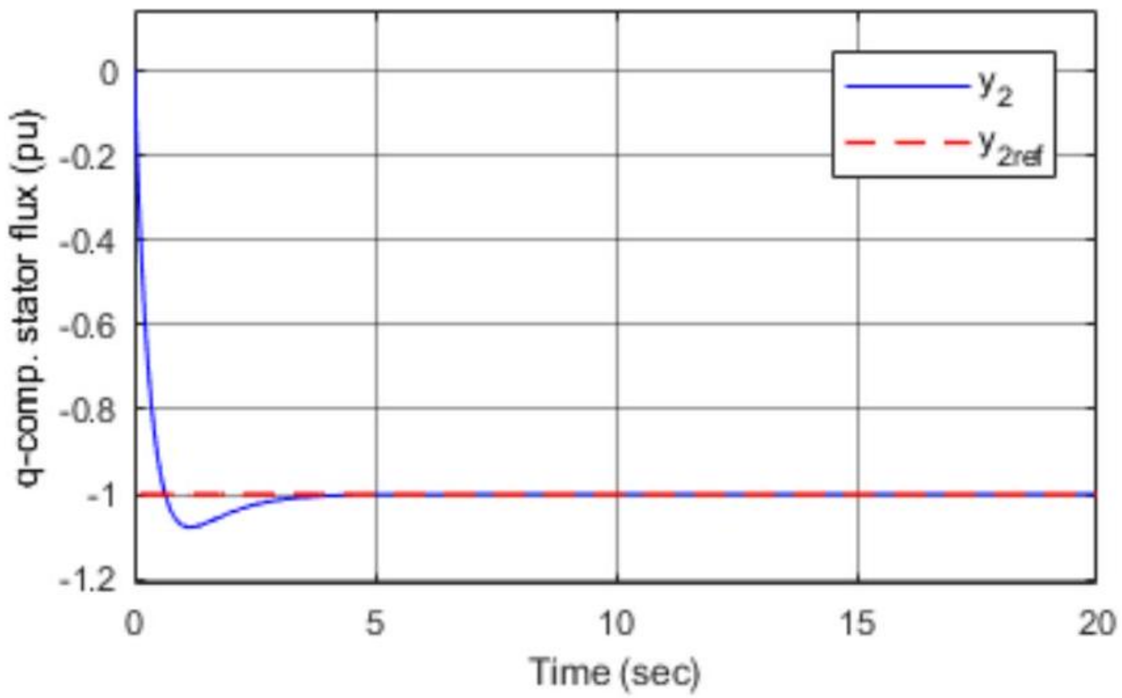

Fig. 5. d-component of stator flux

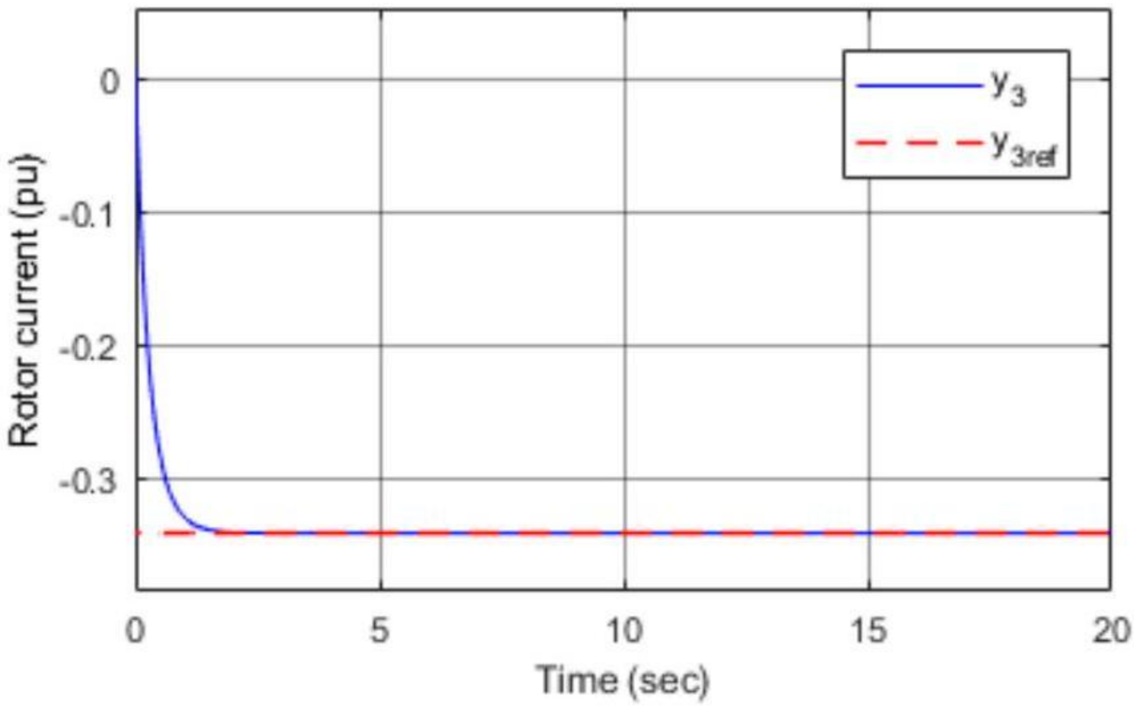

Fig. 6. q-component of rotor current

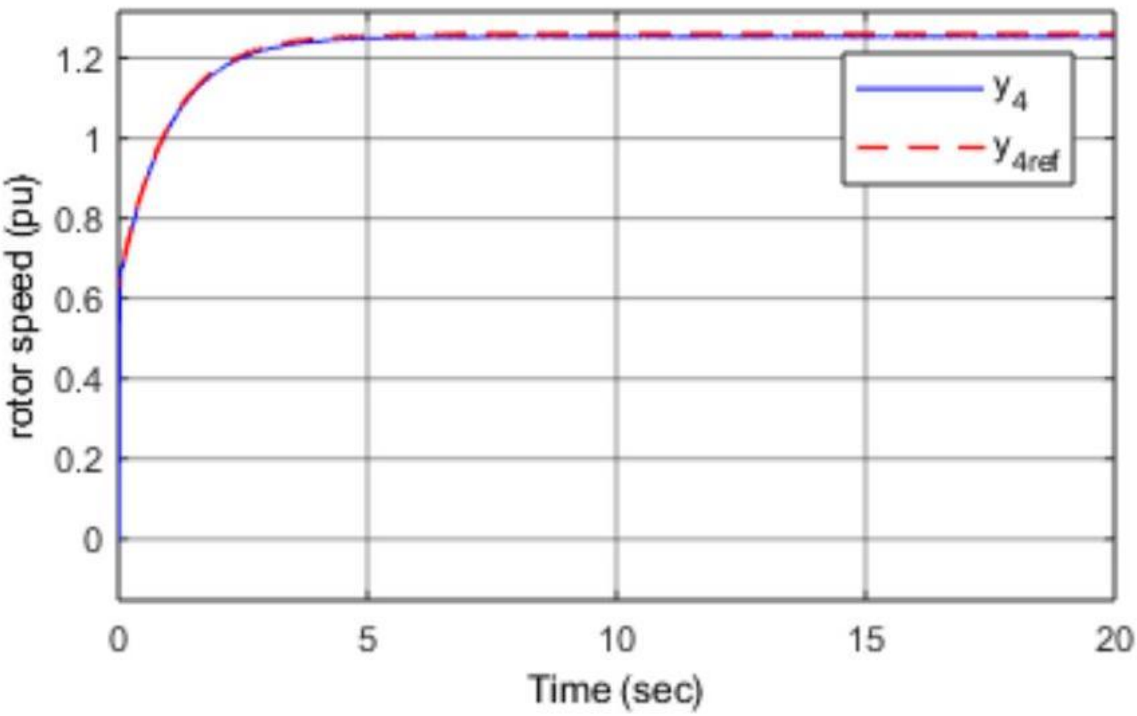

Fig. 7. Optimal rotor speed tracking

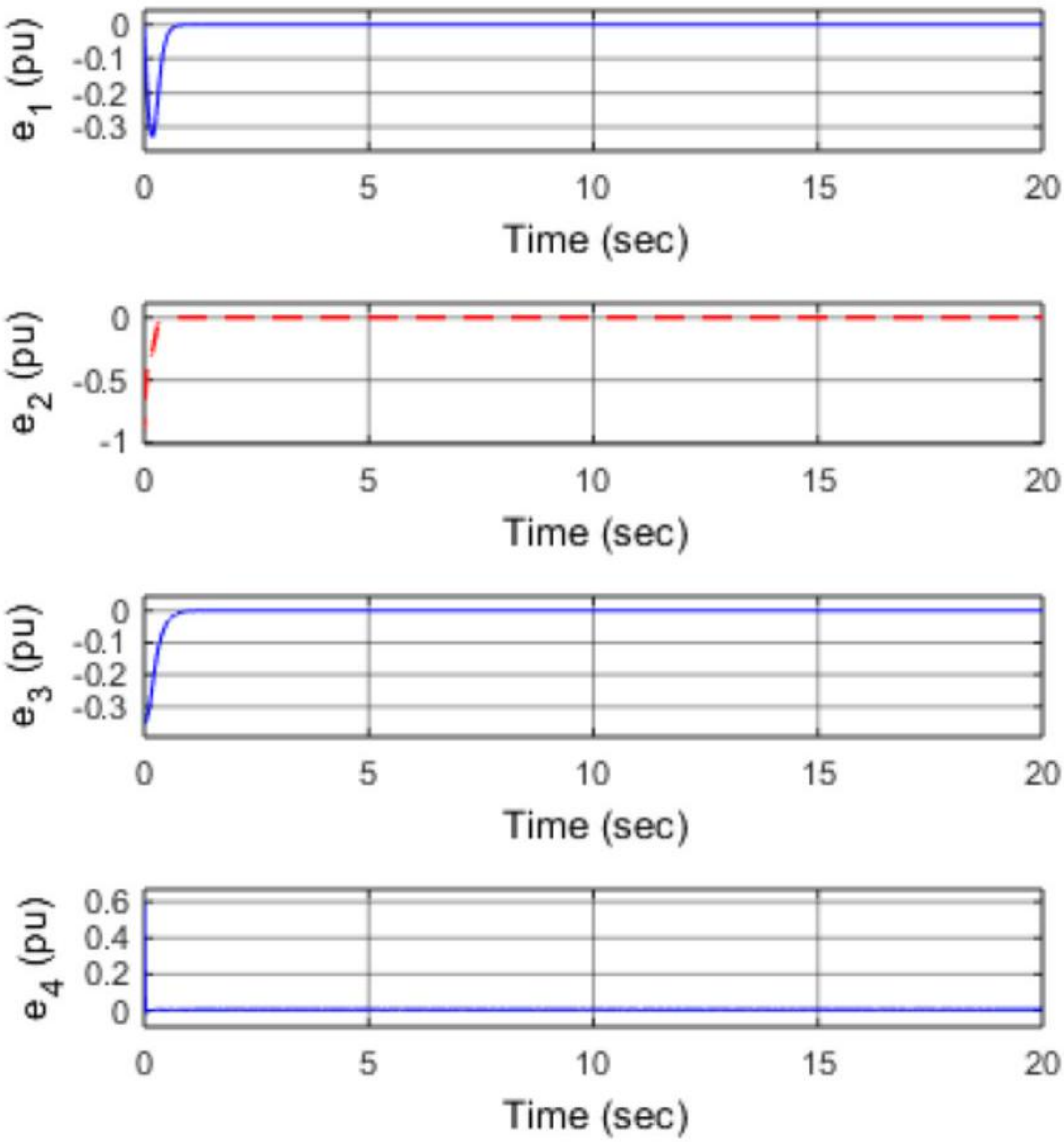

Fig. 8. Tracking errors

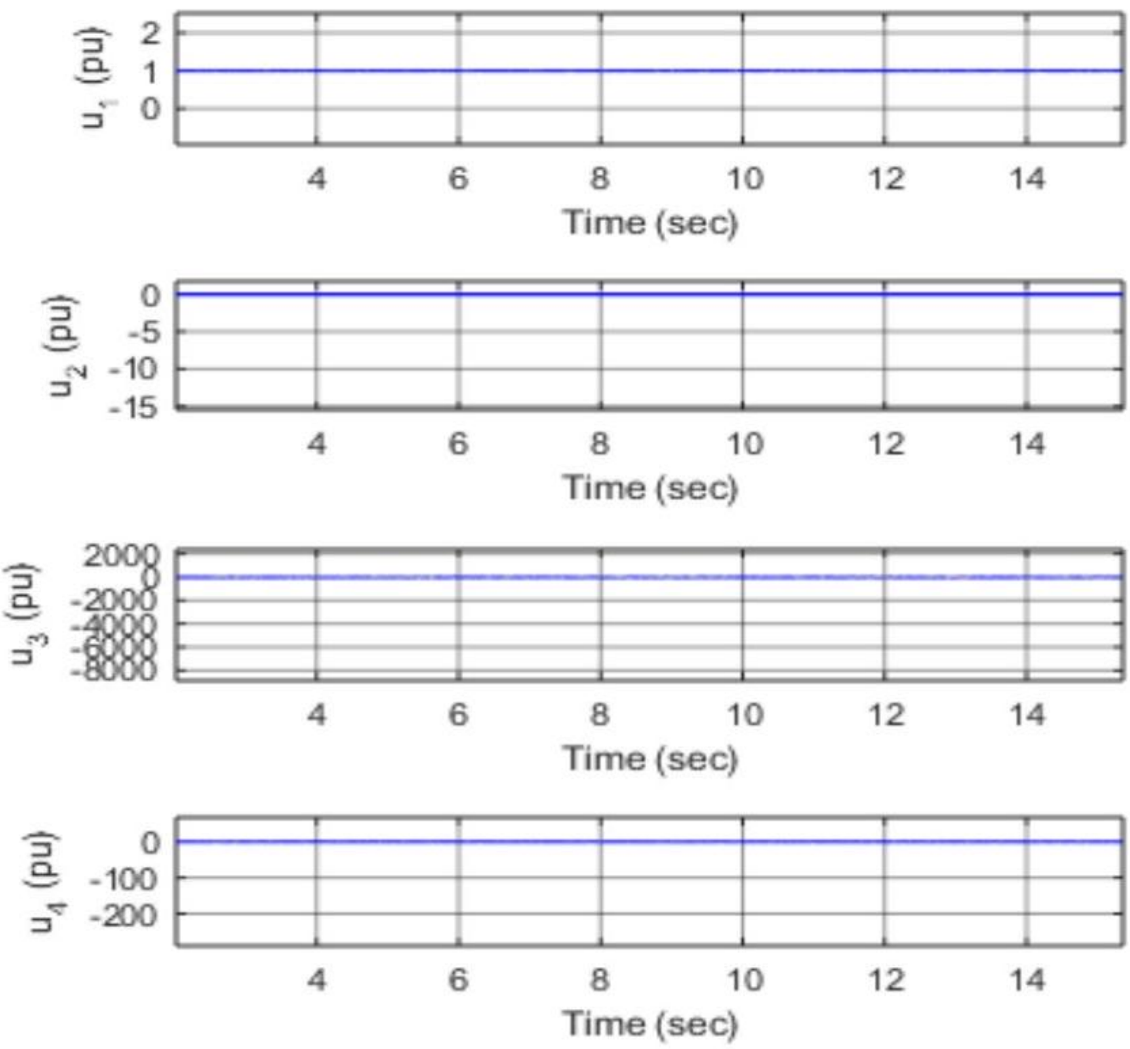

Fig. 9. Control inputs to the DFIG-WT

IX. CONCLUSION

A feedback linearization controller has been used to decouple and linearize the DFIG-WT system. The rotor current and stator flux have been coordinated to regulate the rotor speed to an optimal level. At this speed, the wind turbine can capture the maximum amount of energy. Tracking the optimal rotor speed for MPPT takes time, and there is some overshoot in the rotor speed [34].

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